

4-A1

$$\tau = \frac{T}{\frac{\pi d^3}{16}} = \frac{3 \times 10^6 \text{ (Nmm)}}{\frac{\pi \times 60^3}{16} \text{ (mm}^3\text{)}} = 70.7 \text{ MPa}$$

4-A2

(1)ねじりモーメント

$$T = \frac{60}{2\pi} \cdot \frac{L}{n} = \frac{60}{2\pi} \cdot \frac{7.5 \times 10^3}{120} = 597 \text{ Nm}$$

(2)ねじり応力

$$\tau = \frac{T}{\frac{\pi d^3}{16}} = \frac{597 \times 10^3}{\frac{\pi \times 35^3}{16}} = 70.9 \text{ MPa}$$

4-A3

(1)ねじりモーメント

$$T = \frac{60}{2\pi} \cdot \frac{L}{n} = \frac{60}{2\pi} \cdot \frac{3.7 \times 10^3}{40} = 883 \text{ Nm}$$

(2)ねじり応力

$$\tau = \frac{T}{\frac{\pi d^3}{16}} = \frac{883 \times 10^3}{\frac{\pi \times 50^3}{16}} = 36.0 \text{ MPa}$$

(3)ねじれ角

$$\varphi = \frac{T\ell}{GJ_p} = \frac{883 \times 10^3 \times 300}{80 \times 10^3 \times \frac{\pi \times 50^4}{32}} = 0.00540 \text{ rad (0.309}^\circ\text{)}$$

4-A4

(1)ねじり応力

$$\tau_{AC} = \frac{T_1 - T_2 + T_3}{\frac{\pi d_1^3}{16}} = \frac{(5 - 2 + 3) \times 10^6}{\frac{\pi \times 75^3}{16}} = 72.4 \text{ MPa}$$

$$\tau_{CD} = \frac{-T_2 + T_3}{\frac{\pi d_2^3}{16}} = \frac{(-2 + 3) \times 10^6}{\frac{\pi \times 50^3}{16}} = 40.7 \text{ MPa}$$

$$\tau_{DB} = \frac{T_3}{\frac{\pi d_3^3}{16}} = \frac{3 \times 10^6}{\frac{\pi \times 45^3}{16}} = 168 \text{ MPa}$$

(2)ねじれ角

$$\begin{aligned} \varphi_C &= \frac{(T_1 - T_2 + T_3)a}{Gl_{p1}} = \frac{(5 - 2 + 3) \times 10^6 \times 400}{80 \times 10^3 \times \frac{\pi \times 75^4}{32}} \\ &= 0.00966 \text{ rad } (0.553^\circ) \end{aligned}$$

$$\begin{aligned} \varphi_D &= \varphi_C + \frac{(-T_2 + T_3)b}{Gl_{p2}} = 0.00966 + \frac{(-2 + 3) \times 10^6 \times 600}{80 \times 10^3 \times \frac{\pi \times 50^4}{32}} \\ &= 0.0219 \text{ rad } (1.25^\circ) \end{aligned}$$

$$\begin{aligned} \varphi_B &= \varphi_D + \frac{T_3c}{Gl_{p3}} = 0.0219 + \frac{3 \times 10^6 \times 200}{80 \times 10^3 \times \frac{\pi \times 45^4}{32}} \\ &= 0.0405 \text{ rad } (2.32^\circ) \end{aligned}$$

4-B1

(1)ねじり応力

$$\tau_{AC} = \frac{2T + 3T}{Z_p} = \frac{5T}{Z_p}$$

$$\tau_{CB} = \frac{3T}{Z_p}$$

(2)ねじれ角

$$\varphi_C = \frac{(2T + 3T) \ell / 3}{GI_p} = \frac{5 T \ell}{3 GI_p}$$

$$\varphi_B = \varphi_C + \frac{3T \frac{2}{3} \ell}{GI_p} = \frac{11 T \ell}{3 GI_p} \left(= \frac{2T \ell / 3}{GI_p} + \frac{3T \ell}{GI_p} \right)$$

4-B2

$$\varphi_C = \frac{(2T + T) \ell / 2}{6GI_p} = \frac{T \ell}{4GI_p}$$

$$\varphi_B = \varphi_C + \frac{T \ell / 2}{GI_p} = \frac{3 T \ell}{4 GI_p}$$

4-B3

右端から距離 x の点の直径 d と I_p

$$d = \frac{x}{\ell}(d_2 - d_1) + d_1$$

$$I_p = \frac{\pi}{32} d^4 = \frac{\pi}{32} \left[\frac{x}{\ell}(d_2 - d_1) + d_1 \right]^4$$

x 点の微小幅 dx のねじれ角 $d\varphi$

$$d\varphi = \frac{T dx}{GI_p}$$

従って、全体のねじれ角は全長で積分して求める。

$$\begin{aligned} \varphi &= \int_0^\ell \frac{T dx}{GI_p} = \frac{32T}{\pi G} \int_0^\ell \frac{1}{\left[\frac{x}{\ell}(d_2 - d_1) + d_1 \right]^4} dx \\ &= \frac{32T\ell(d_1^2 + d_1 d_2 + d_2^2)}{3\pi G d_1^3 d_2^3} \end{aligned}$$

4-B4

<つり合いの式>

$$T_A + T_B = T$$

<変形の式>

$$\varphi_B = \frac{(T - T_B)\ell/2}{3GI_p} - \frac{T_B \ell/2}{GI_p} = 0$$

よって、 $T_B = \frac{1}{4}T$, $T_A = \frac{3}{4}T$

$$\varphi_C = \frac{(T - T_B)\ell/2}{3GI_p} = \frac{T\ell}{8GI_p} \left(= \frac{T_A \ell/2}{3GI_p} \right)$$

4-B5

$$\varphi_B = \frac{TS_0}{4A^2tG} \frac{2}{3} \ell + \frac{T}{G} \frac{\ell}{\frac{bt^3}{3}} = \frac{8T\ell}{3\pi d^3tG} + \frac{T\ell}{\pi dt^3G}$$

4-B6

(1)ねじりモーメント

$$T = P \cdot \ell = 100 \times 150 = 15000 \text{ Nmm}$$

(2)ボルトの径

$$d = \sqrt[3]{\frac{16T}{\pi\tau_a}} = \sqrt[3]{\frac{16 \times 15000}{\pi \times 50}} = 11.5 \text{ mm}$$